

April 1st, 2025

Electrochemical and thermochemical-based processes for production of chemicals

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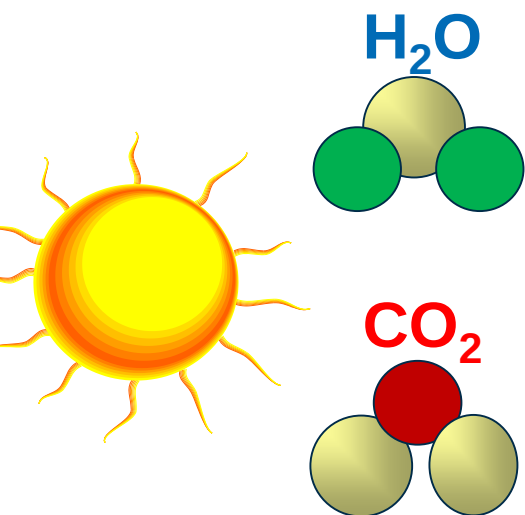
**Politecnico
di Torino**



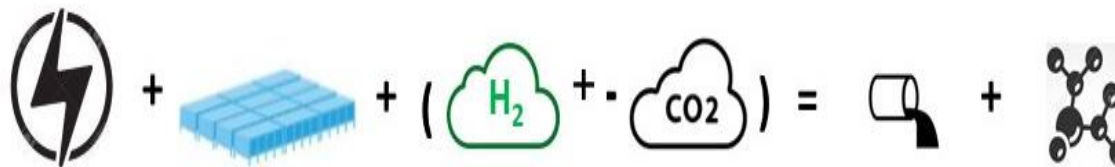
- **Electrochemical processes** (high and low temperature electrolysis, fuel cells, closed batteries, redox flow batteries, e-metals, power-to-power systems, plasma processes)
- **Thermochemical processes** (chemical looping, thermocatalysis, solar chemicals)
- **CO₂ capture and conversion** (membranes and ionic liquids, chemical looping)
- **e-chemicals**
- **solar chemicals**

<https://youtu.be/qUxnzP2J4yk>

e-pathway towards platform molecules



Electrochemical conversion



Thermochemical conversion

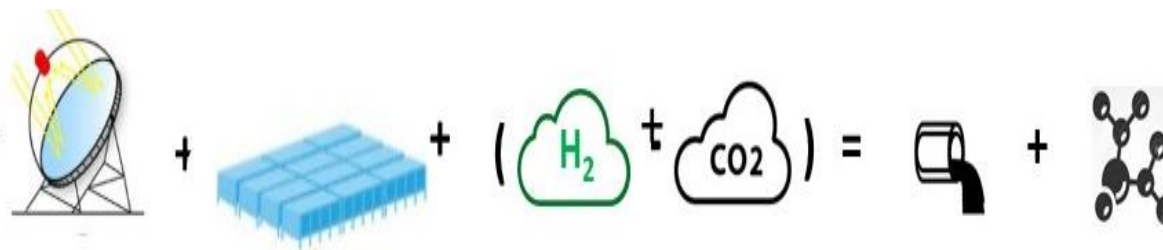
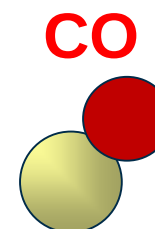
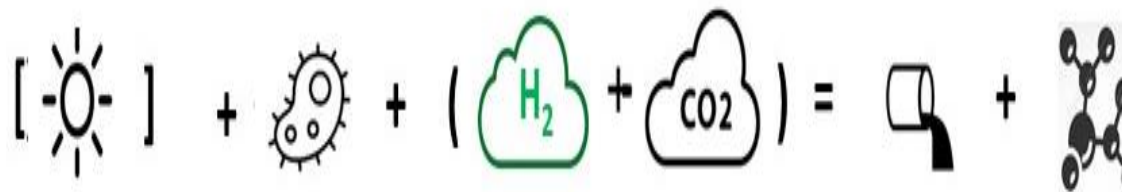


Photo-catalytic conversion



Biological conversion

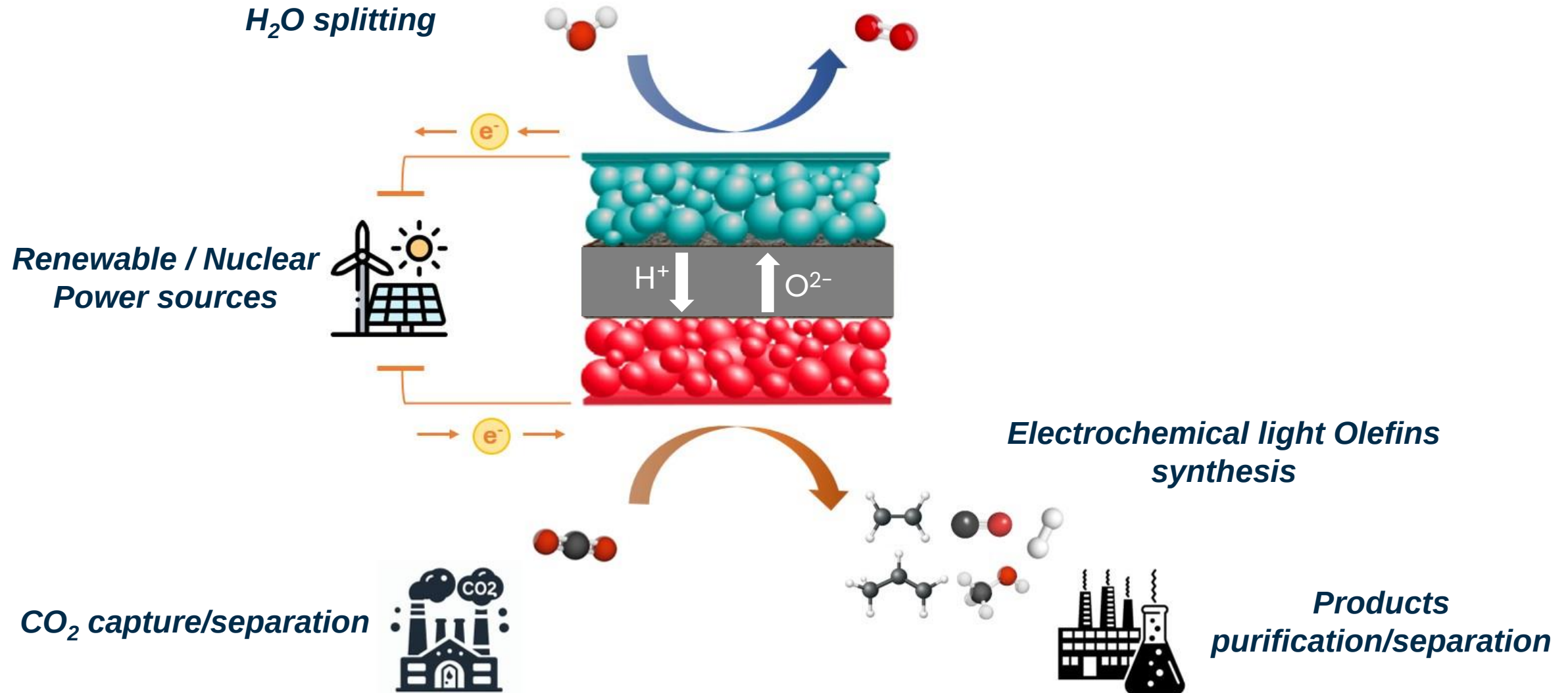


P
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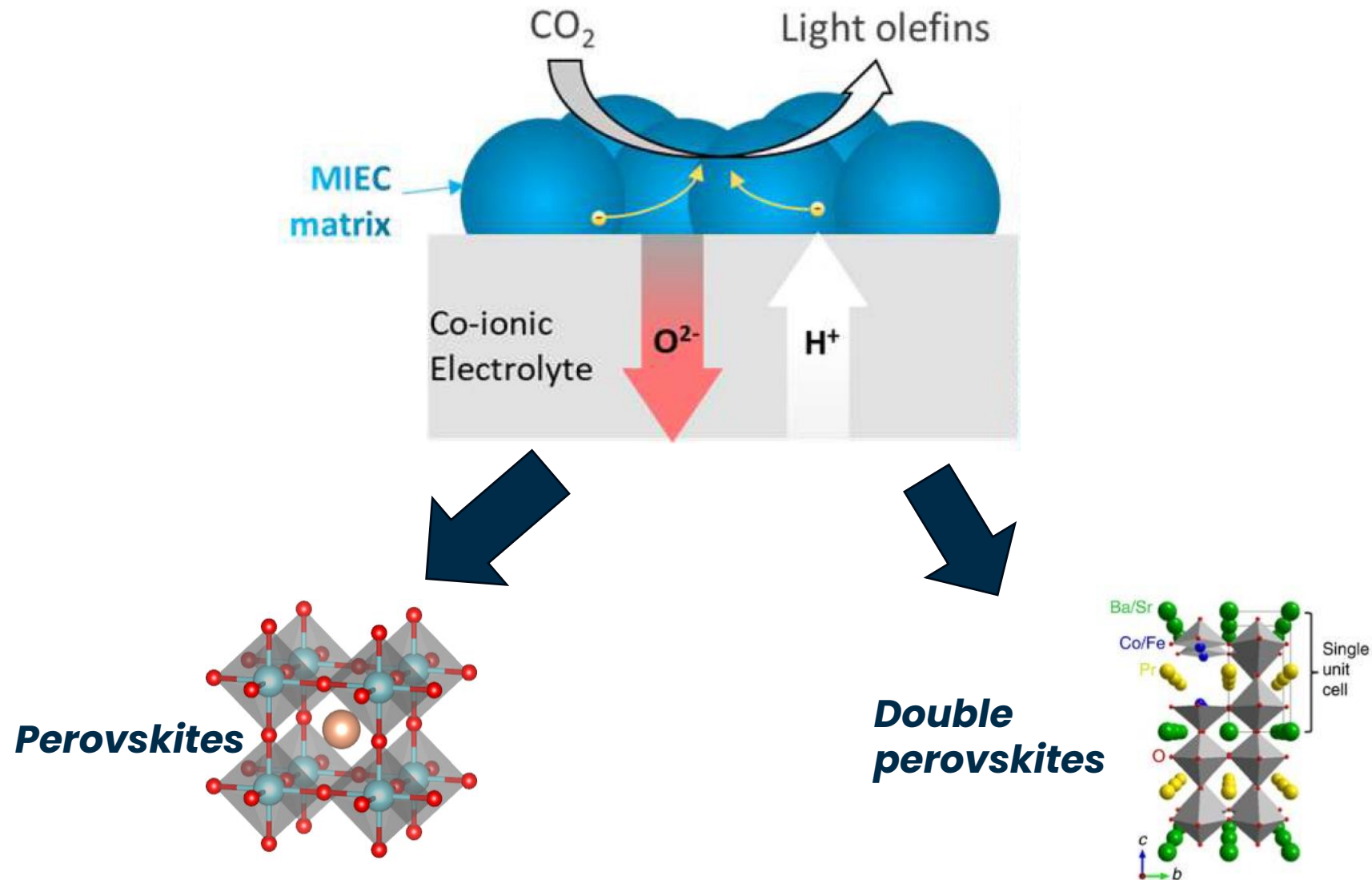
M
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Co-ionic ($\text{H}^+ + \text{O}^{2-}$) ceramic membranes

Nano-Engineered Co-Ionic Ceramic Reactors for $\text{CO}_2/\text{H}_2\text{O}$ Electro-conversion to Light Olefins



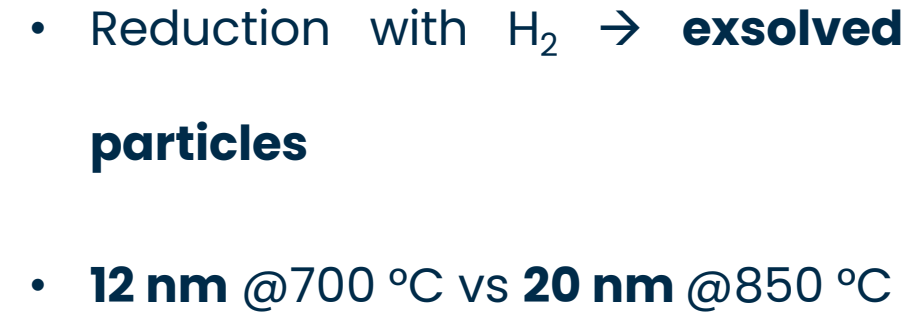
Development of Cathode Materials: *Triple conducting (H^+ , O^{2-} , e^-) oxides matrices*





Post-TPR 700 °C

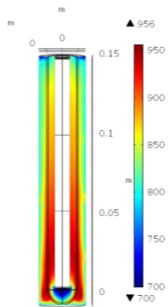
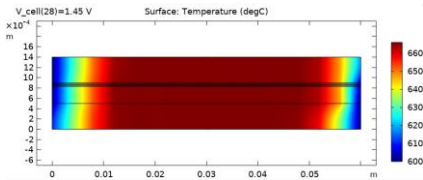
Post-TPR 850 °C



SFNM turns into a perovskite-like phase $\text{Sr}_3\text{MoO}_{6-\delta}$, along with the exsolution of a Ni-Fe-rich alloy
Strong catalytic effect on CO_2 reduction

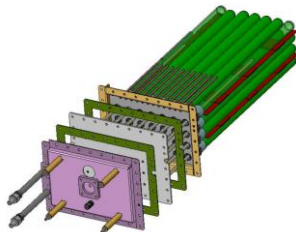
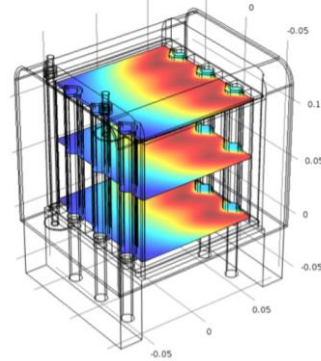
Cell model

2D planar+tubular



SRU/Stack model

3D planar+tubular



Ionic transport in the membrane (Nernst-Planck-Poisson governing equations)

Defect conservation equation

$$\frac{\partial [X_k]}{\partial t} + \nabla \cdot J_k = \omega_k$$

Defect transport flux (Nernst-Planck)

$$J_k = -D_k(\nabla[X_k] + \frac{z_k F}{RT} [X_k] \nabla \phi_e)$$

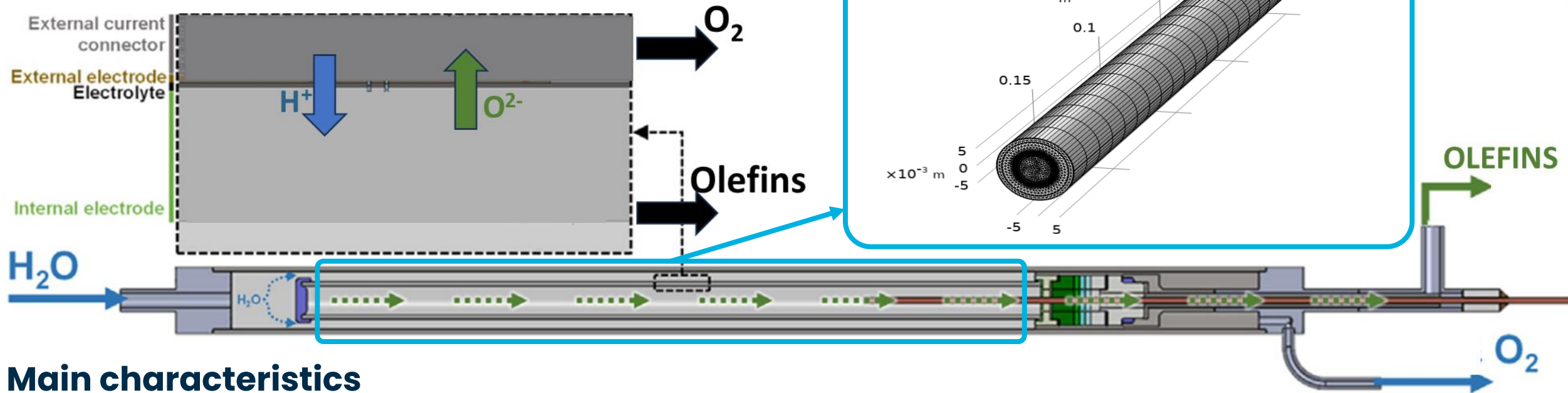
Gauss Law

$$\nabla \cdot (\epsilon_r \epsilon_o \nabla \phi) = -\rho = -F \sum z_k [X_k]$$

Conductivity (Nernst-Einstein)

$$\sigma = \frac{F^2}{RT} \sum_{k=1}^K z_k^2 [X_k] D_k$$

- **Tubular SRU model**



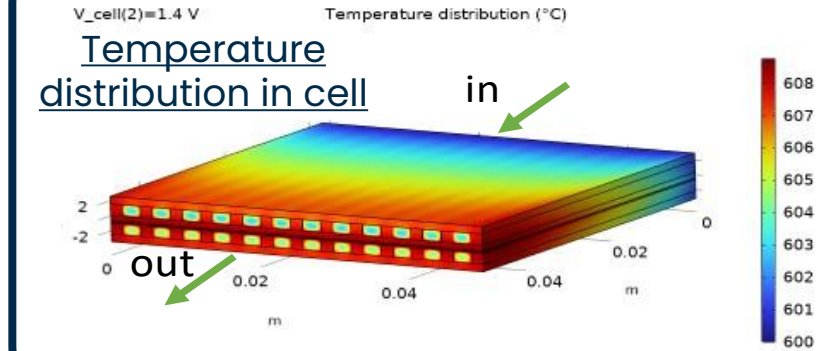
Main characteristics

- Tube in shell configuration leading to sealed chambers:
 - Internal chamber with olefins production (avoids olefins dilution and allows recirculation)
 - External chamber with by-product (oxygen recovery with economic valorization)
- Porous conductive medium between electrode and external shell (lower losses and higher area)
- Self-contained modular sub-assembly for easier scaling and integration into larger systems

CFD model development and simulations of the ci-EMR cells/stacks

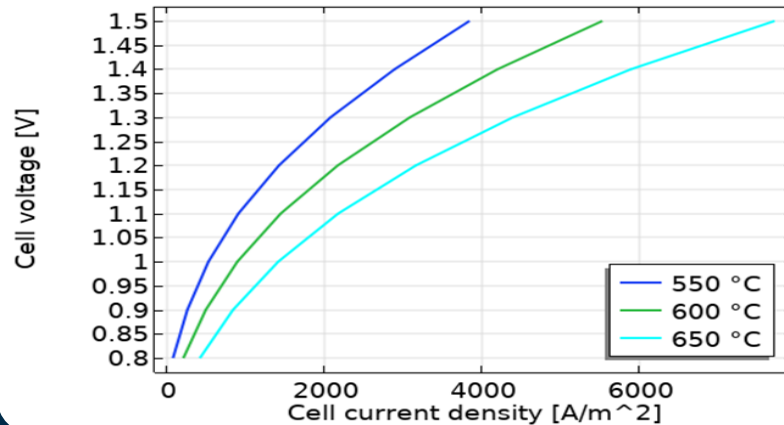
- **Planar SRU modelling**

- 3D geometries
- Implementation of thermal model

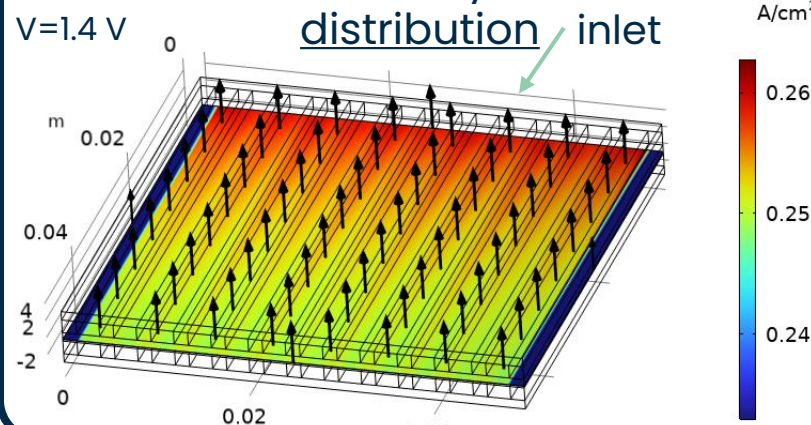


Results

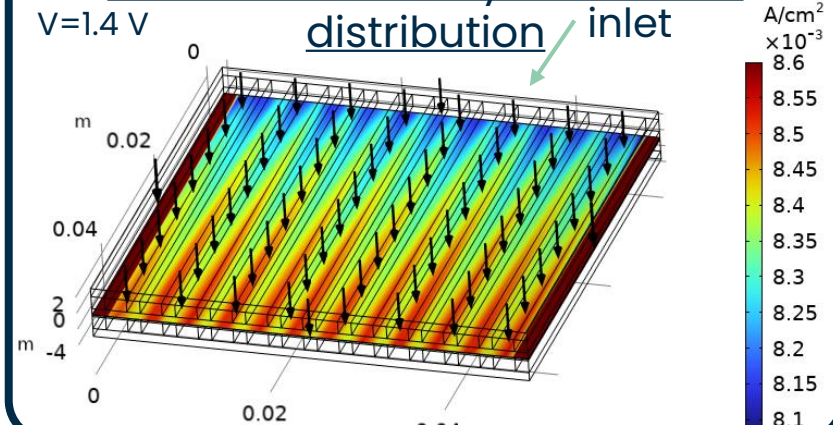
Polarization curves



H^+ current density volumetric distribution



O^{2-} current density volumetric distribution



Boundary Conditions

- Cell size = $5 \times 5\text{ cm}^2$
- $T_{\text{inlet,gas}} = T_{\text{cell}}$
- $p = p_{\text{atm}}$
- Imposed potential

Cathode

$$i_{0,HER} = 1.39 \cdot 10^7\text{ A/m}^2 \cdot e^{\frac{-48.12 \cdot 10^3\text{ J/mol}}{R \cdot T}}$$

Anode

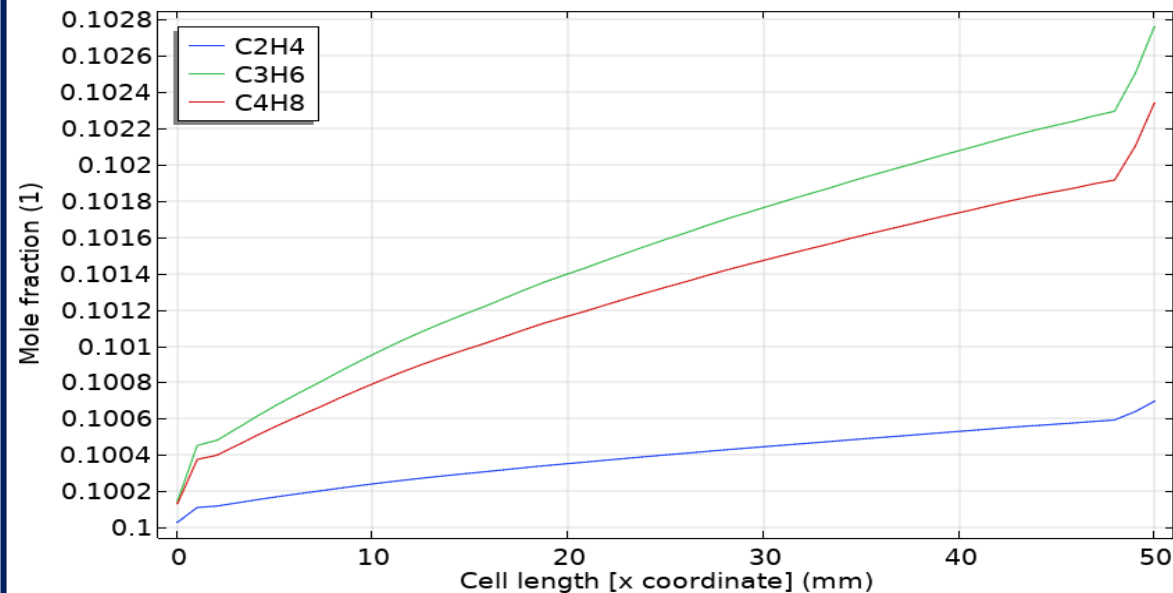
$$i_{0,OER} = 5.38 \cdot 10^{11}\text{ A/m}^2 \cdot e^{\frac{-180 \cdot 10^3\text{ J/mol}}{R \cdot T}}$$

Electrochemical olefins production

- CO₂ electro-hydrogenation to light-olefins** enhanced by co-ionic membranes



Olefins molar fraction over cell length (V=1.9V)



- Co-ionic reactions** at the electrodes only linked to the overall conductivity

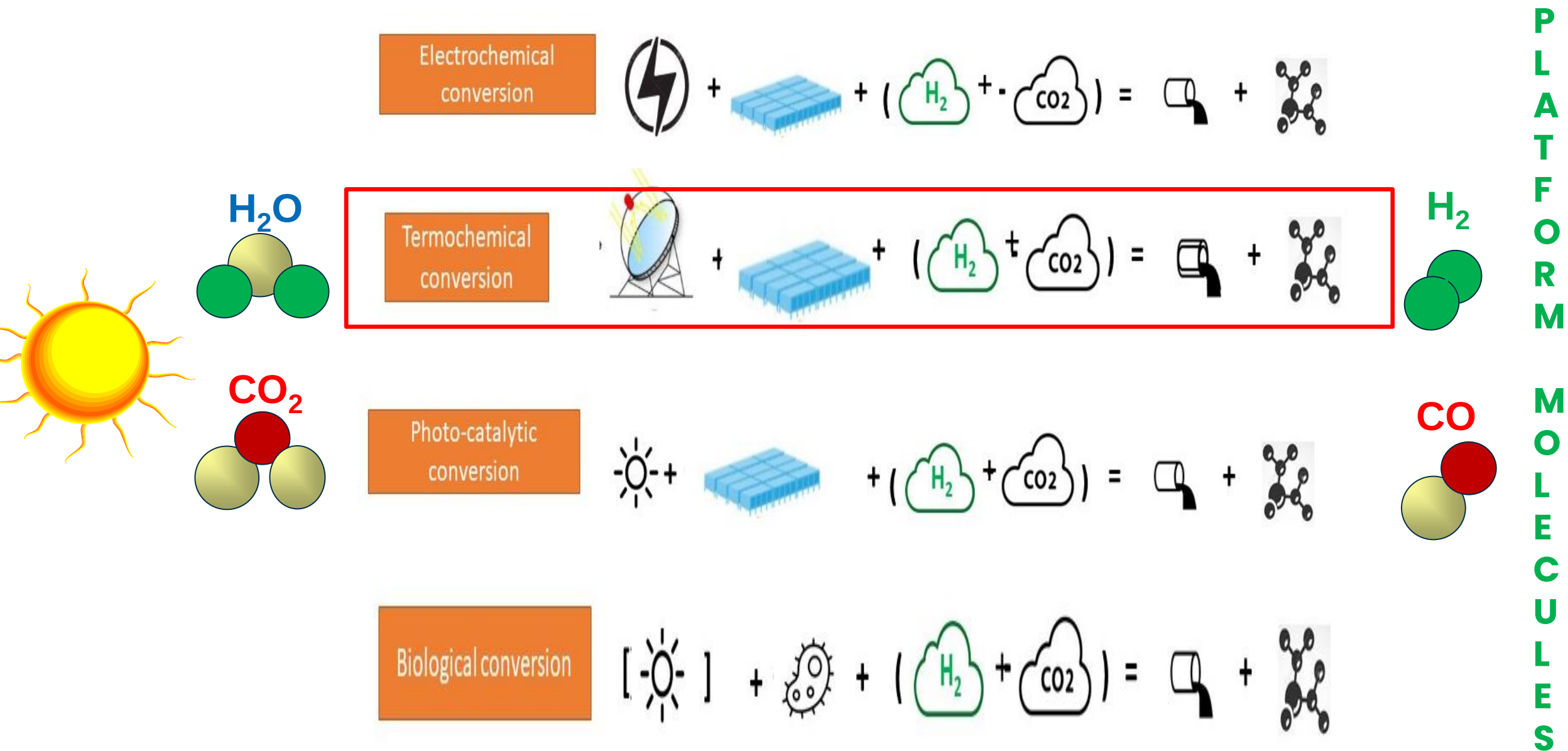
- Improvements currently evaluated:**

- Relation between partial current density of single defect and Butler-Volmer

$$i_{loc} = i_0 \left(\exp\left(\frac{\alpha_a F \eta}{RT}\right) - \exp\left(\frac{-\alpha_c F \eta}{RT}\right) \right)$$

- Variable pre exponential term of the Butler-Volmer

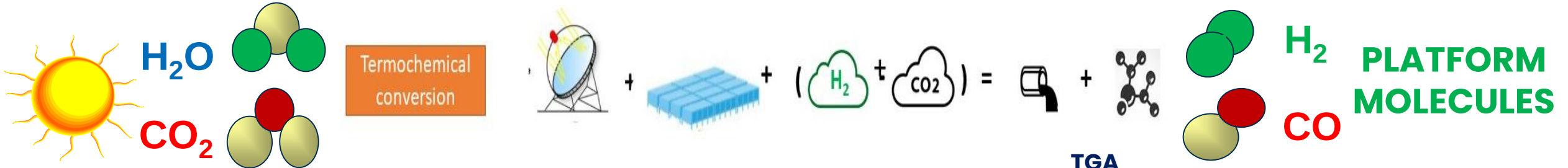
thermal-pathway towards platform molecules



PLATFORM MOLECULES

PLATFORM MOLECULES

Chemical Looping based H₂O/CO₂ conversion



Materials explored for Chemical Loopir

20%CeO₂-80%Fe₂O₃
 La_{0.75}Sr_{0.25}CoO₃
 La_{0.75}Sr_{0.25}FeO₃
 70% Fe₂O₃-30% Al₂O₃
 80% Fe₂O₃-Ce_{0.5}Zr_{0.5}O₂
 25%LSF-SiO₂
 50%LSF/SBA-15
 La_{0.5}Ca_{0.5}Fe_{0.25}Mn_{0.75}O₃
 LaCo_{0.25}Fe_{0.50}Mn_{0.25}O₃
 Gd_{0.3}Ce_{1.7}O_{2-δ} (GDC)/Fe₂O₃
 La_{0.75}Sr_{0.25}FeO₃-encapsulated
 Co₃O₄-NiO
 La_{0.8}Sr_{0.2}FeO₃
Sr₂FeNi_{0.4}Mo_{0.6}O₆

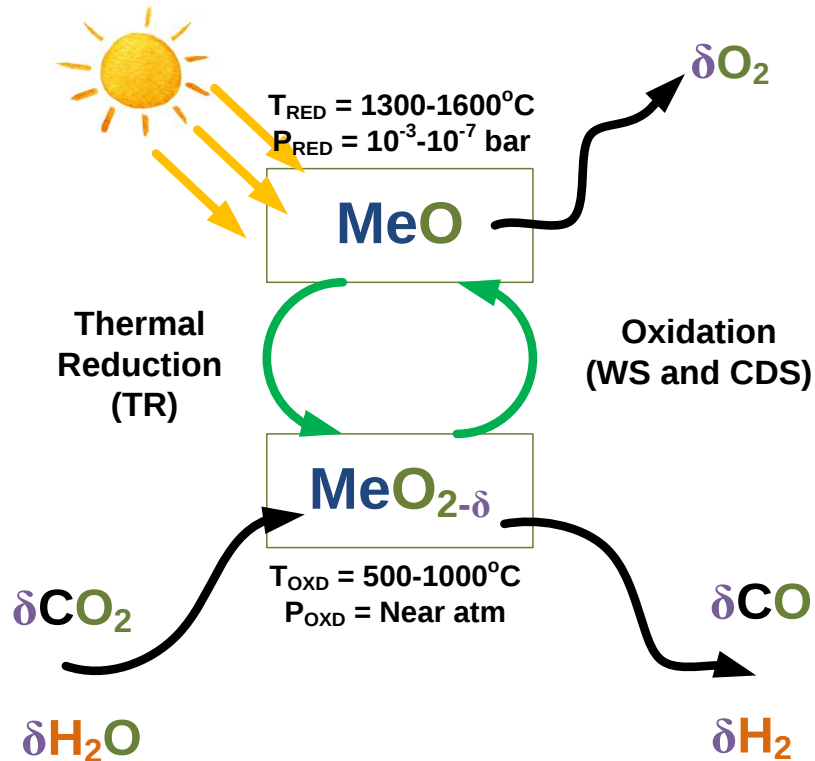
TGA



REACTOR



SOLAR CONCENTRATOR

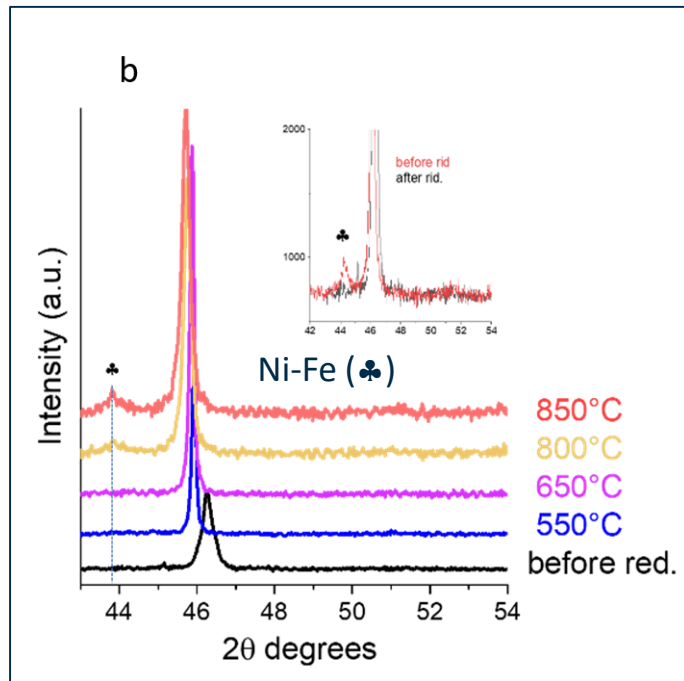
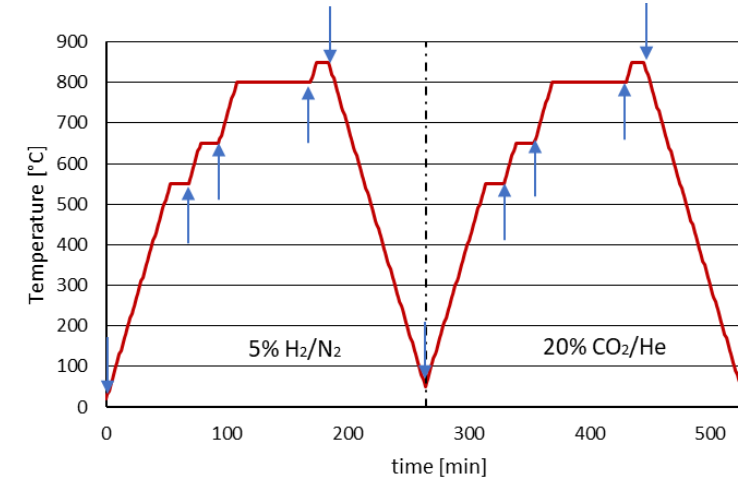


❖ **Sr₂FeNi_{0.4}Mo_{0.6}O₆ (SFNM) for Chemical Looping**

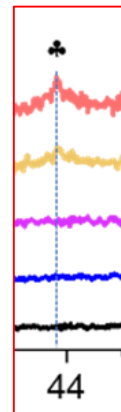
Experimental activity: structural evolution vs T

✓ Investigating the **structural evolution vs temperature**

- Temperature Programmed Reduction (**TPR**)
- *In situ* X-Ray Diffraction (**HC-XRD**)
- Diffractograms at 50, 550, 650, 800, 850 °C (*blue arrows*)
- Reduction: 5% H₂/N₂



TPR – Metal alloy exsolution



Ni-Fe alloy (♣) detected for T > 800 °C (*downstream, observed deriving from an exsolution process*)

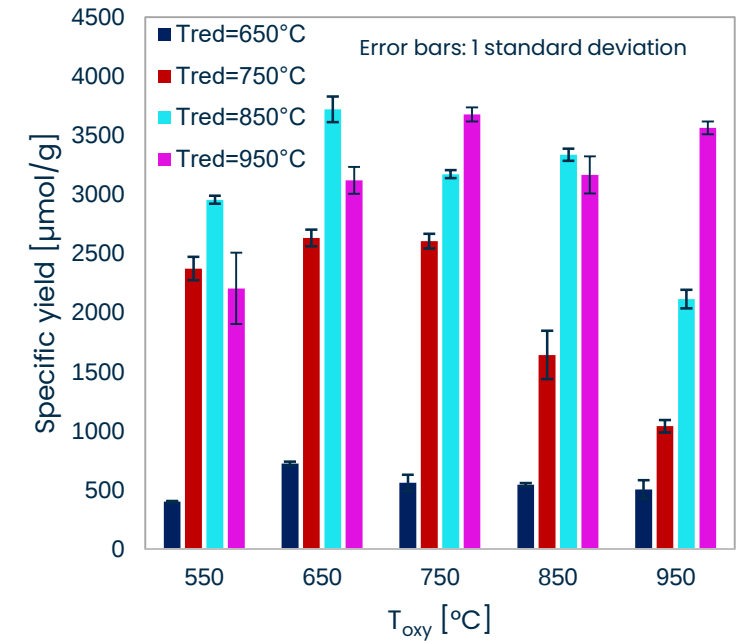
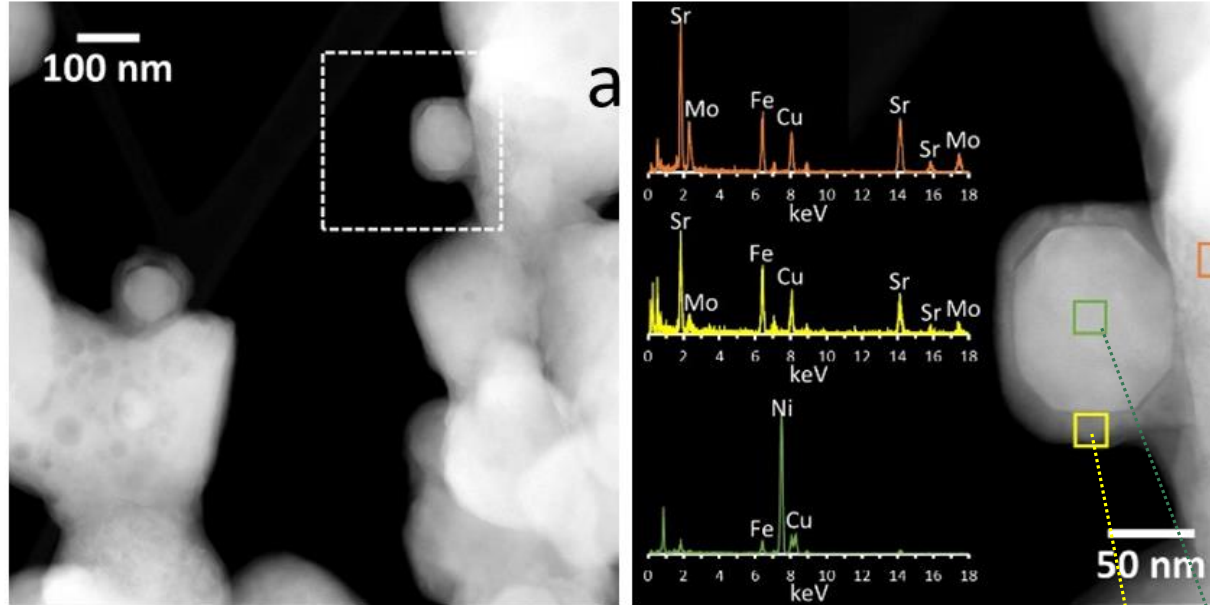
Experimental activity: long tested samples

- Long-tested sample was analysed via HAADF-STEM, HRTEM and EDX

Exsolution-enhanced reverse water-gas shift chemical looping activity of $\text{Sr}_2\text{FeMo}_{0.6}\text{Ni}_{0.4}\text{O}_{6-\delta}$ double perovskite

Francesco Orsini, Domenico Ferrero, Salvatore F. Cannone, Massimo Santarelli, Andrea Felli, Marta Boaro, Carla de Leitenburg, Alessandro Trovarelli, Jordi Llorca, Georgios Dimitrakopoulos, Ahmed F. Ghoniem

[Chemical Engineering Journal, Volume 475, 1 November 2023, 146083](#)



- Exsolution leads to the formation of **core-shell structures**
- The core contains **Ni-Fe**, while the matrix and the shell contain **Sr, Mo (some Fe)**
- The **exsolved core-shell structure appears to be very redox-active**

Ni-Fe core

Perovskite-like shell

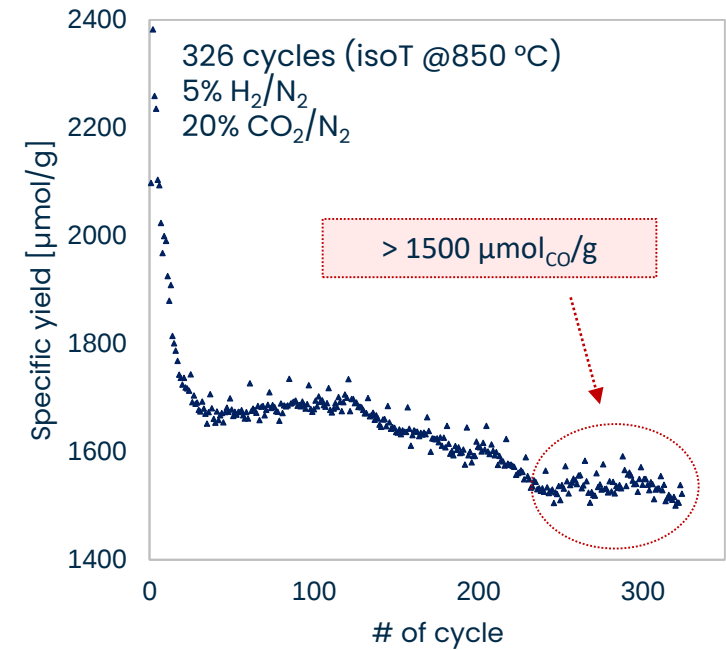
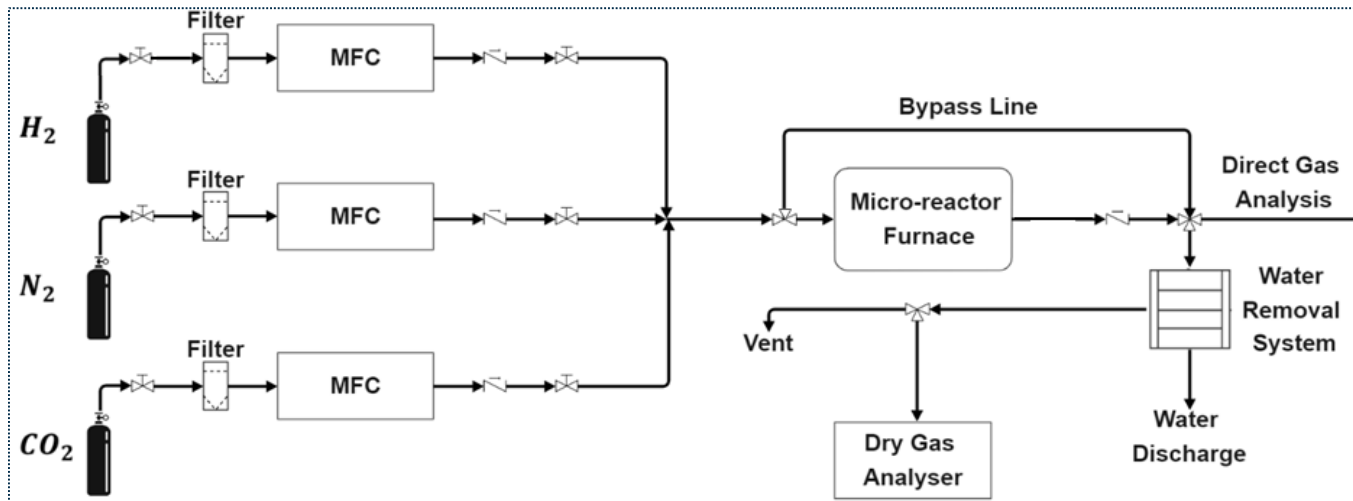
Optimal temperatures for maximizing the CO yield:

- $T_{\text{red,opt}} \approx 850^{\circ}\text{C}$
- $T_{\text{oxy,opt}} \approx 650^{\circ}\text{C}$

Experimental activity: SFNM redox stability (I)

✓ Assessing the material **stability** and CO yield **repeatability**

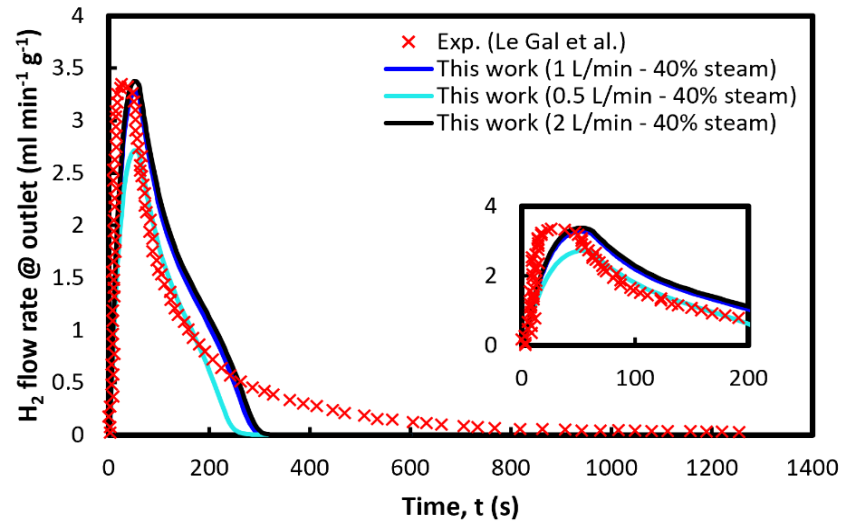
- Long-duration stability was explored through **320+ isothermal cycles** at **850 °C** (optimal T from previous tests)
- 5% H₂/N₂ – 20% CO₂/N₂
- Fixed-bed reactor coupled with online gas analysis (scheme below)



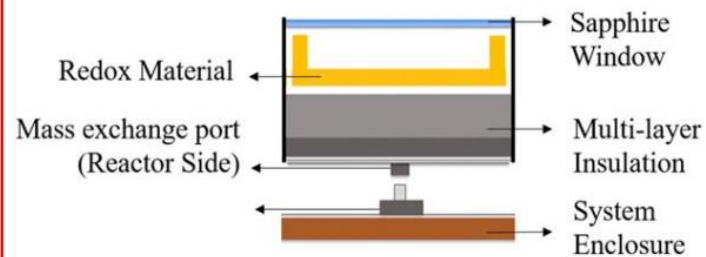
- Yield flattens out at > 1500 μmol_{CO}/g
- Long-tested SFNM thus seems to ensure good redox performances

Scale-up and future concept

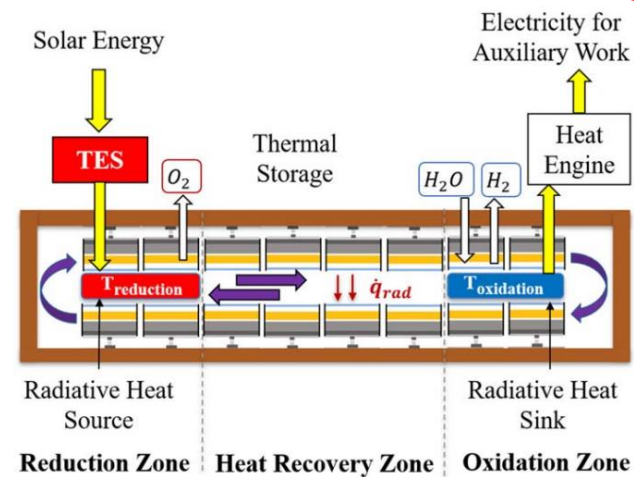
- Testing receiver/reactor in solar concentrator



«Train Reactor» configuration



Collaboration with MIT



Tubular fixed-bed

Mass and momentum conservation (Brinkman)

$$\frac{\partial}{\partial t}(\epsilon_p \rho) + \nabla \cdot (\rho \mathbf{u}) = Q_m$$

$$\frac{\rho}{\epsilon_p} \left(\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \frac{\mathbf{u}}{\epsilon_p} \right) = -\nabla p + \nabla \cdot \left[\frac{1}{\epsilon_p} \left\{ \mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \frac{2}{3} \mu (\nabla \cdot \mathbf{u}) \mathbf{I} \right\} \right] - \left(\frac{\mu}{\kappa} + \frac{Q_m}{\epsilon_p^2} \right) \mathbf{u}$$

Chemical species transport (Chapman-Enskog)

$$D_i^f = \left(\sum_{j=1}^n \frac{x_j}{D_{ij}} \right)^{-1} \quad D_{ij} = \frac{0.00266 T^{\frac{3}{2}}}{p M_{ij}^{\frac{1}{2}} \sigma_{ij}^2 \Omega_D} \quad M_{ij} := 2 \left[\left(\frac{1}{M_i} \right) + \left(\frac{1}{M_j} \right) \right]^{-1} \quad \{i, j = \text{Ar}, \text{O}_2\}$$

Local Thermal Non-Equilibrium

$$\left. \begin{aligned} (1 - \epsilon_p) \rho_s c_{p,s} \frac{\partial T_s}{\partial t} + \nabla \cdot \mathbf{q}_s &= q_{sf}(T_f - T_s) + (1 - \epsilon_p) Q_s \\ \epsilon_p \rho_f c_{p,f} \frac{\partial T_f}{\partial t} + \rho_f c_{p,f} \mathbf{u} \cdot \nabla T_f + \nabla \cdot \mathbf{q}_f &= q_{sf}(T_s - T_f) + \epsilon_p Q_f \end{aligned} \right\} \quad \begin{aligned} q_{sf} &= h_{sf} A_{sf} \\ &\text{(literature correlations} \\ &\text{for dual scale RPC)} \end{aligned}$$

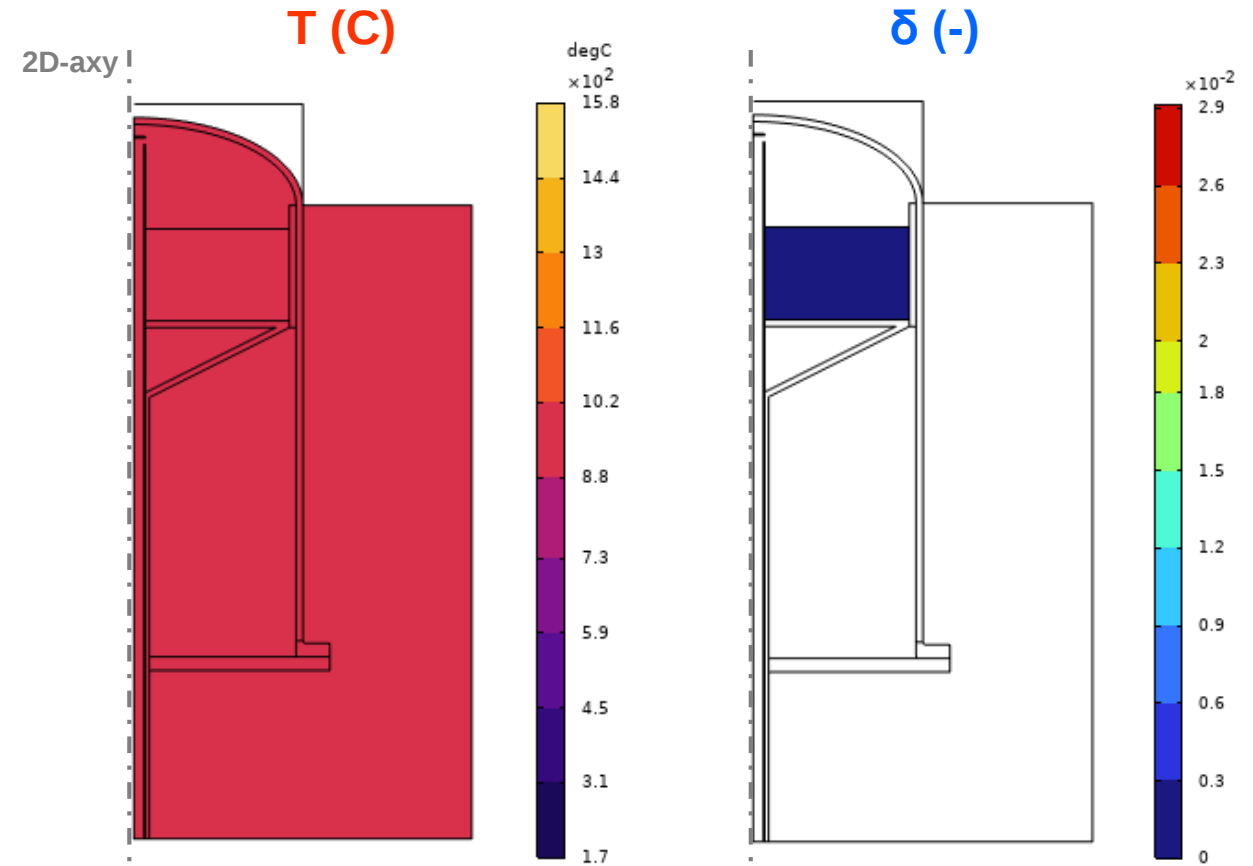
Internal radiative heat transfer (P1 approx.)

$$\nabla \cdot (-D_{p1} \nabla G) = -\kappa(G - 4\pi I_b)$$

$$G = \int_{4\pi} I(\Omega) d\Omega, \quad D_{p1} = \frac{1}{3\kappa + \sigma_s(3 - a_1)}$$

Redox thermodynamics

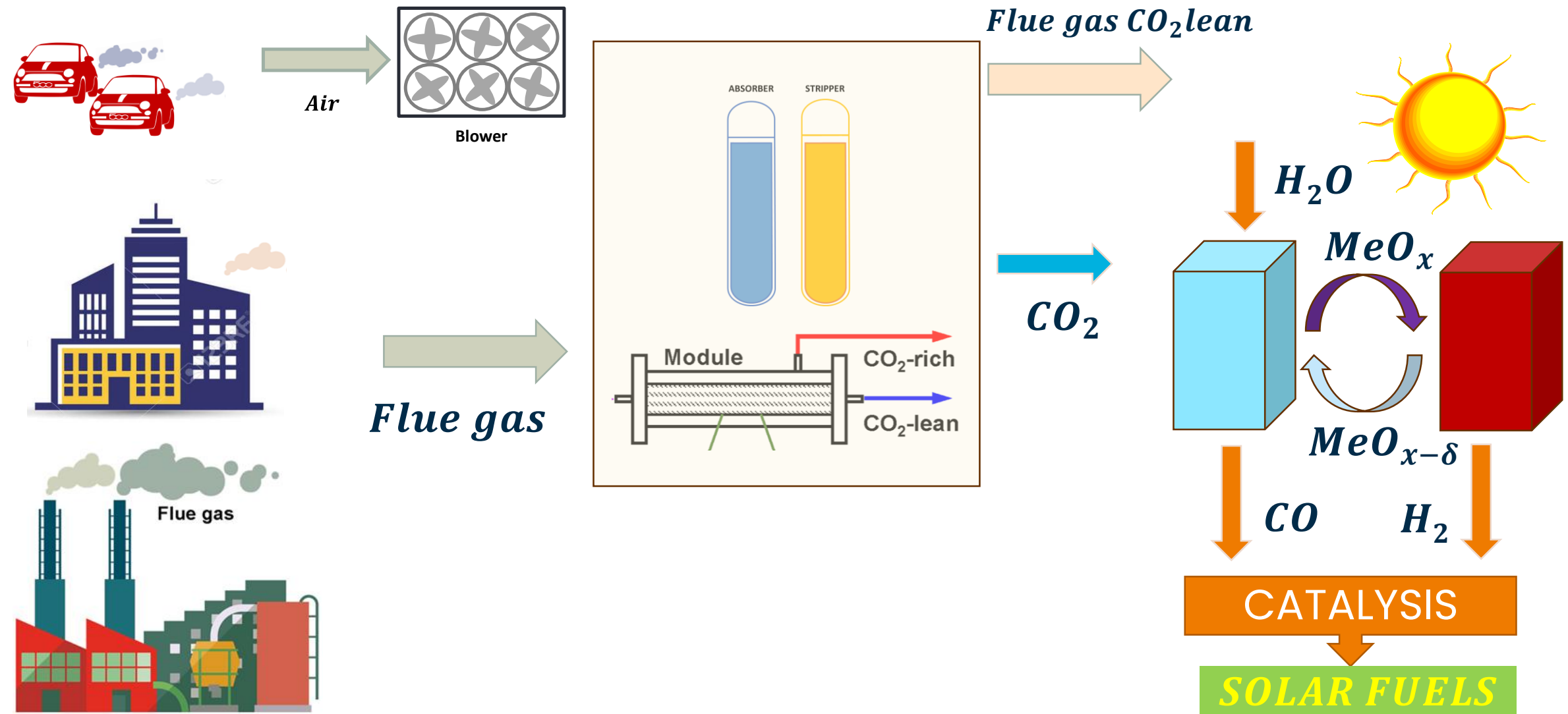
$$\delta_{\infty}(T, p_{\text{O}_2}) = \delta_{\max} \frac{8700 p_{\text{O}_2}^{\text{no}_2} e^{-\frac{195.6 [\text{kJ mol}^{-1}]}{R_g T}}}{1 + 8700 p_{\text{O}_2}^{\text{no}_2} e^{-\frac{195.6 [\text{kJ mol}^{-1}]}{R_g T}}}, \quad \delta(t=0) = 0$$



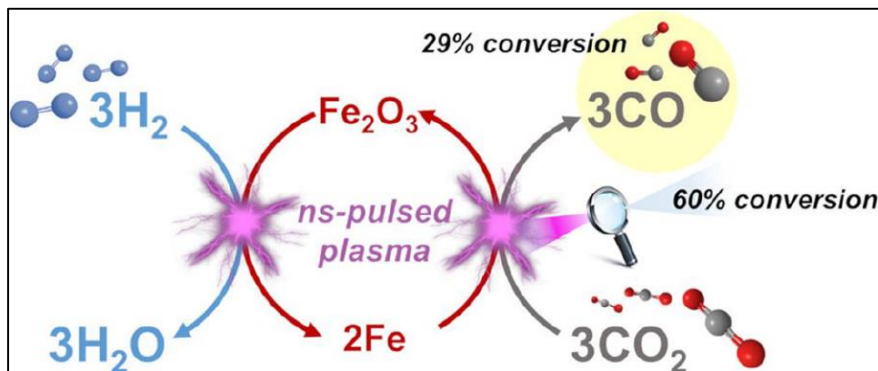
1 hour simulation results.

- The model will be used to:
 - Compare different operational regimes (e.g., sweep vs vacuum)
 - Explore the effect of the porous medium morphology
 - Couple reduction and oxidation models via consistent initial conditions in the fluid domains

Scale-up and future concept



Improving CO₂ Conversion by Plasma-Assisted Chemical Looping



Plasma-based set-ups can be combined with a **packing material**, usually referred to as **plasma-catalysis**

Experimental setup:

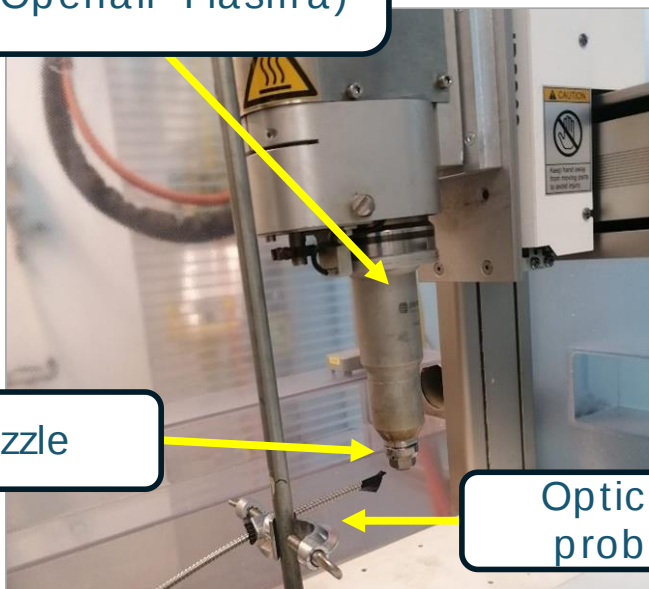
cold plasma is used to **dissociate CO₂**.

Reduced SFNM material, placed downstream of the plasma, is expected to capture oxygen to **prevent CO recombination**

Plasma Torch
(Openair- Plasma)

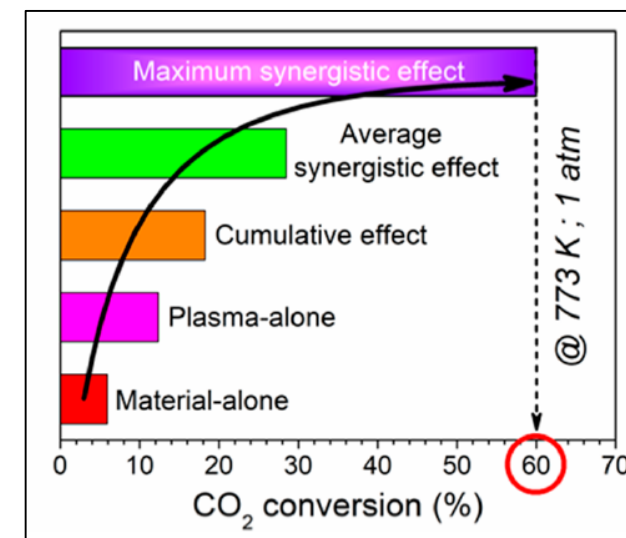
Nozzle

Optical probe



Main expectations:

achieved up to 60% instantaneous CO₂ conversion in plasma: the process exhibited a 2-4-fold increase in CO₂ conversion compared to plasma or material alone*





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